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CHARACTERIZATION OF POLYVINYLIDENE FLUORIDE

Final Report

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Characterization of Polyvinylidene Fluoride

by

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The research accomplished through the partial or complete support of ARO grant number DAHCO4-75G-0083 can be stated briefly in the following outline.

- An apparatus for the measurement of the electrical properties of polymer films was designed and constructed.
- 2) A procedure was developed and an apparatus modified for the bulk polymerization of ultrapure poly(vinylidene fluoride) (referred to hereafter as PVF₂).
- 3) The dielectric properties of a series of films made from both our own ultrapure polymer and commercial polymer were determined and compared.
- 4) Pyroelectric current and depolarization current measurements were performed on both samples of our own polymer which we had poled ourselves and on poled samples which were supplied to us by the Kureha and Pennwalt companies.
- 5) A corona poling device was designed and constructed to allow for better poling than we were able to achieve with the apparatus to be described in section one.

Electrical Apparatus

The electrical apparatus was designed with versatility in mind. The heart of the apparatus is the sample cell, shown schematically in Figures 1, 2 and 3. This cell can be used with a capacitance bridge to determine

the dielectric properties of polymer films or with an electrometer to measure their dc conductivities or current phenomena (thermally stimulated currents, pyroelectric currents, depolarization currents). Sample poling can also be done in this cell. Temperature regulation for the apparatus is provided by a Eurotherm temperature controller and programmer combination. With this sample cell the temperature can be ramped linearly in mV from -196° C to 250° C at rates between 0.1 and 6.25° /min and has a long term stability of $\sim 0.1^{\circ}$ C. A full description of the sample cell may be found in the 1/77-6/77 report.

As well as the sample cell, which was used for all the electrical measurements to be described in subsequent sections, the grant partially supported the construction of an automatic dielectrometer which can measure sequentially the real and imaginary parts of the dielectric constant at four frequencies (50,500,5000,50,000 Hz). The output is connected to a chart recorder which records both dielectric and temperature data. A sample output is shown in Figure 4. A detailed description of the dielectrometer may be found in reference 1.

Radiation Polymerization

Commercial samples of poly(vinylidene fluoride) were found to contain significant quantities of potentially ionizable impurities grafted onto the polymer chain. In order to distinguish the electrical properties intrinsic to poly(vinylidene fluoride) from those caused by impurities, we felt it was important to find a bulk polymerization procedure which yielded ultrapure polymer. The technique chosen, radiation induced polymerization, was originally investigated by Doll and Lando². A high vacuum rack was modified

to serve as a monomer distillation and degassing apparatus. For homopolymer, vinylidene fluoride monomer was triply distilled into a stainless steel reaction vessel and degassed with several freeze-evacuate-melt sequences. The final pressure at 80° K was $\sim 10^{-5}$ Torr. For P(VF-VF₂) copolymer, 5% triply distilled vinyl fluoride by volume was added to the reaction vessel before degassing. After degassing the reaction vessel was warmed to the polymerization temperature and placed in a cobalt 60 y radiation source. Sixty percent conversion of monomer to homopolymer required a 0.8 Megarad dose. This technique produced ultra high molecular weight polymer-on the order of three to six million as estimated from intrinsic viscosity measurements. The intrinsic viscosities (dl/gm) of PVF_2 homopolymer and $P(VF-VF_2)$ copolymer determined in N,N-dimethyl acetamide were found to be 5.5 and 5.2 respectively while that of commercial polymer with a molecular weight of 140,000 was approximately 1. The high molecular weight of our polymers made them practically intractable. Pressing high quality thin films was virtually impossible. For this reason a study of molecular weight and head to head content as a function of polymerization (temperature) conditions was begun. This work as well as work on reducing the molecular weight of the polymer through addition of chain transfer agents has been continued under ARPA grant DAAK-70-77-C-0055 and the results will be published shortly. Dielectric Measurements

Dielectric measurements were carried out on the series of homemade and commercial films listed in Table 1. The films were gold shadowed on both sides and placed in the sample cell described in a previous section. A General Radio capacitance bridge was used to determine the dielectric proper-

Table 1

Sample	Phasea	Source	Film Preparation
A	11	Pennwal t	Melt pressed from repre- cipitated Pennwalt pellets.
В		Pennwalt	Melt pressed from Penn- walt pellets coprecipi- tated with 5% poly(vinyl fluoride).
C	11	Kureha	As received KF capacitor grade film.
D	1,11	CWRU	Melt pressed homopolymer.
E	- 11	CWRU	Melt pressed homopolymer.
F	1	CWRU	Melt pressed P(VF-VF ₂) copolymer.

a. Determined from WAXD scans.

ties (dielectric constant and loss tangent) of films A, B and D at 100, 1000, 10,000 and 100,000 Hz. The results are shown in Figures 5-10. Figures 11-16 show the results for films C, E and F determined with the automatic dielectrometer. Several points can be made in comparing the results from homemade and commercial films.

The low temperature β transition which normally occurs at approximately -70°C at 110 Hz³ and is attributed the local oscillation of frozen main chains, is not observable for any of the films.

The α_a transition, due to the onset of micro-Brownian motion of the amorphous chain segments at the glass transition temperature, can be seen clearly for all the films. The room temperature dielectric constants for the two films made from Pennwait pellets (A and B shown in Figures 5 and 7)

are lower than those of the other films.

The high temperature $\alpha_{\mbox{\scriptsize c}}$ transition produced by molecular motion in the crystalline regions is evident in some but not all of the spectra. It can be seen clearly in Figures 10,14 and 17 which show tan δ for films D and E and an expanded view of tan δ for film F. These are all films of radiation polymerized PVF2. A hint of the transition can also be found in the tan δ plot for the Pennwalt homopolymer film a (Figure 6) but there is no evidence of it in either the Kureha KF film or the Pennwalt polymer blend. The α_c transition in the commercial films may be obscured by contribution of ionic impurities to the high temperature dielectric properties. Both the dielectric constant and the loss tangent for the Pennwalt films (A and B, Figures 5-8) increase much more rapidly as a function of temperature than those of the other films. Figures 18 and 19 show a comparison of the dielectric properties (dielectric constant and tan & respectively) for radiation polymerized homopolymer (film E), copolymer (film F) and commercial Kureha film (film C) at 50 Hz. In Figure 18 we see that the dielectric constants of the two phase II films (C and E) are similar and have a greater temperature dependence than that of the phase I film. However, comparison of the loss tangents (Figure 19) shows a considerable difference between the CWRU samples and the Kureha film clearly demonstrating the low levels of ionic impurities present in radiation polymerized samples.

Pyroelectric and Depolarization Measurements

A number of attempts were made to pole films pressed from our radiation polymerized homo and copolymers and to measure their resultant pyroelectric properties. One such homopolymer film, recrystallized in the sample chamber

under a field gradient of 50 KV/cm, gave a small but observable pyroelectric effect (~ 10⁻¹¹C/°cm²) while a copolymer film recrystallized under a 120 KV/cm field gradient had a pyroelectric coefficient of $2-3 \times 10^{-10}$ C/°cm² between 70° and 120°C. The pyroelectric response of the latter film was unaffected by annealing at 165°C. This is in marked contrast another copolymer film which was poled at 130° and 300 KV/cm for 30 min. The pyroelectric coefficient of this film as a function of temperature and annealing time is shown in Figure 20. Similar curves obtained for samples of experimental PVF₂ provided to us already poled from Pennwalt and Kureha are shown in Figures 21 and 22. It can be seen from these curves that initially the pyroelectric coefficient rises steeply with increasing temperature. After annealing, however, it becomes practically independent of temperature. This behavior suggests to us that the pyroelectric response of poly(vinylidene fluoride) may be composed of two parts: a temperature dependent part which may be annealed out leaving only the temperature independent part. We postulate that the temperature independent part of the pyroelectric response may be due to the classical dipole mechanism while the temperature dependent part may be due to injected charges which may be annealed out. In order to test this hypothesis, work has continued under the ARPA grant to produce films of our radiation polymerized PVF2 with dipoles aligned by nonelectrical means, thus eliminating all possible pyroelectric mechanisms except the classical dipole mechanism.

An interesting effect in the annealing experiment on the Pennwalt sample was noted in last periods report. One sees in Figure 21 that there is a dip in the high temperature pyroelectric response when the sample is

annealed at 129°C for 545 minutes but the current recovers when the sample is allowed to rest at room temperature over the weekend. An experiment was undertaken to map out the time dependence of this current recovery for a Pennwalt sample. It demonstrated that there is also a recovery of a current, like the initial thermally stimulated current, which is lost irreversibly on the first heating after a rest. The results of the experiment are not well understood and more work will be needed to interpret them.

In addition to the work on the pyroelectric response some effort was expended in looking at depolarization phenomena through measurement of the depolarization current. In at least some of the samples there is an indication that spontaneous polarization may be occurring on annealing rather than depolarization. Again this aspect of the work must be pursued farther in order to arrive at more definite conclusions.

Corona Discharge Poling Apparatus

The values observed for the pyroelectric coefficients of the radiation polymerized PVF2 films, which were poled in the electrical apparatus, were lower than those for the commercially poled samples. This was attributed to the thickness of the melt pressed high molecular weight films and the limited voltage gradient which we could achieve. We, therefore, designed and built a separate corona poling apparatus which would allow us to place higher poling fields across our sample. An exploded view of the sample chamber of this apparatus is shown in Figure 23. A 10,000 volt power supply has been built to supply the voltage across the cell and the progress of the poling is monitored by an electrometer placed across a capacitor in series with the cell. With this apparatus we can routinely achieve voltages of 2-3 million volts per cm for samples of 1 mil capacitor grade Kureha film.

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- 3. H. Kakutani, J. Polym. Sci. A2, 8, 1177-1186 (1970).

Figure Captions

- Figure 1. Sample holder and sample can for dielectric cell.
- Figure 2. Gas inlet arrangement for dielectric cell.
- Figure 3. Dielectric cell.
- Figure 4. Sample output from the automatic dielectrometer. The real and imaginary parts of the dielectric constant (ϵ ' and ϵ '' respectively) for four different measurement frequencies (50 Hz, 500 Hz, 5 KHz and 50 KHz) and the output of the sample thermocouple are recorded on a strip chart recorder.
- Figure 5. The dielectric constant of Pennwalt PVF₂ homopolymer (sample A) as a function of temperature for four measurement frequencies: 1. 100 Hz, 2. 1 KHz, 3. 10 KHz, 4. 100 KHz.
- Figure 6. Tan δ of Pennwalt PVF₂ homopolymer (sample A) as a function of temperature at four measurement frequencies: 1. 100 Hz, 2. 1 KHz, 3. 10 KHz, 4. 100 KHz.
- Figure 7. The dielectric constant of Pennwalt P(VF₂- VF) copolymer (sample B) as a function of temperature for four measurement frequencies:
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 1. 100 Hz, 2. 1 KHz, 3. 10 KHz, 4. 100 KHz.
- Figure 10. Tan δ of CWRU PVF2 homopolymer (sample D) as a function of temperature for four measurement frequencies: 1. 100 Hz, 2. 1 KHz, 3. 10 KHz, 4. 100 KHz.
- Figure 11. The dielectric constant of Kureha PVF₂ homopolymer (sample C) as a function of temperature at four measurement frequencies: 50 Hz, + 500 Hz, 5 KHz, x 50 KHz.
- Figure 12. Tan δ of Kureha homopolymer (sample C) as a function of temperature at four measurement frequencies:

 50 Hz, + 500 Hz,

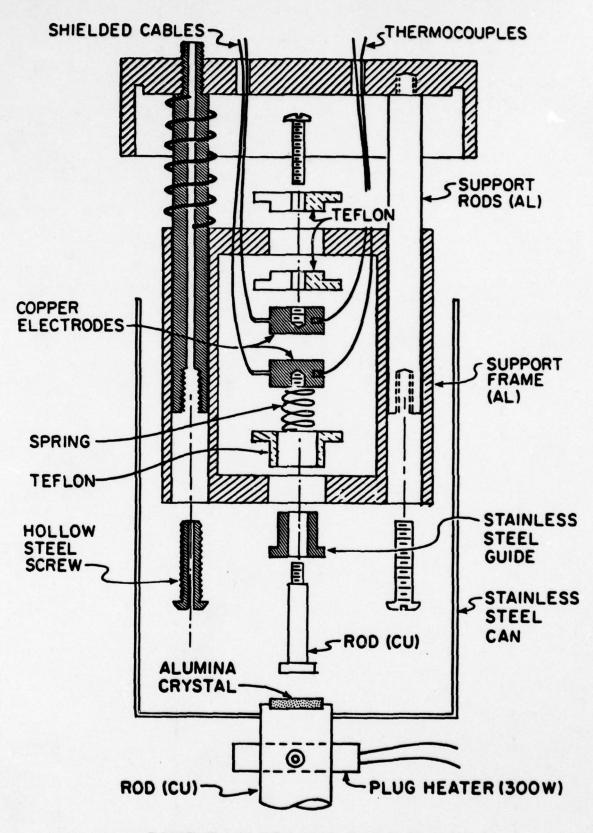
 5 KHz,

 50 KHz.
- Figure 13. Dielectric constant of CWRU PVF₂ homopolymer (sample E) as a function of temperature for four measurement frequencies: 50 Hz, + 500 Hz, 5 KHz, x 50 KHz.
- Figure 14. Tan δ of CWRU homopolymer (sample E) as a function of temperature at four measurement frequencies:

 50 KHz, + 500 Hz,

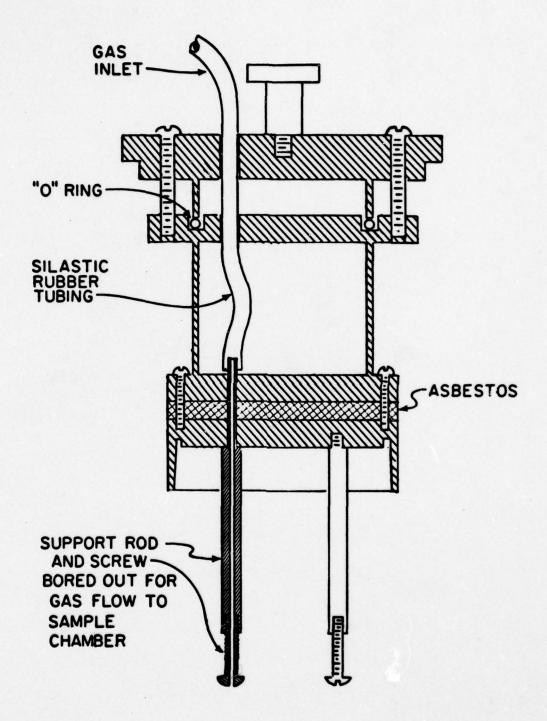
 50 KHz.

- Figure 15. Dielectric constant of CWRU P(VF-VF₂) copolymer (sample F) as a function of temperature for four measurement frequencies: 50 Hz, + 500 Hz, 5 KHz, × 50 KHz.
- Figure 16. Tan δ of CWRU P(VF-VF₂) copolymer (sample F) as a function of temperature for four measurement frequencies: = 50 Hz, + 500 Hz,
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- Figure 19. Comparison of tan δ at 50 Hz for Kureha homopolymer (sample C)
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- Figure 20. Pyroelectric coefficient as a function of temperature and annealing for CWRU P(VF-VF₂) copolymer: o initial run, **p** annealed at 129°C for 50 min., Δ annealed at 129°C for approximately 80 min. and subsequently at 160°C for 1300 min.
- Figure 22. Pyroelectric coefficient for Kureha PVF₂ as a function of temperature and annealing: o as received film uncorrected for thermally stimulated current, x initial run corrected for TSC., Φ annealed at 132°C for 65 min., an annealed at 132°C for 170 min., Δ annealed at 132°C for 1170 min.
- Figure 23. Exploded view of corona poling cell.



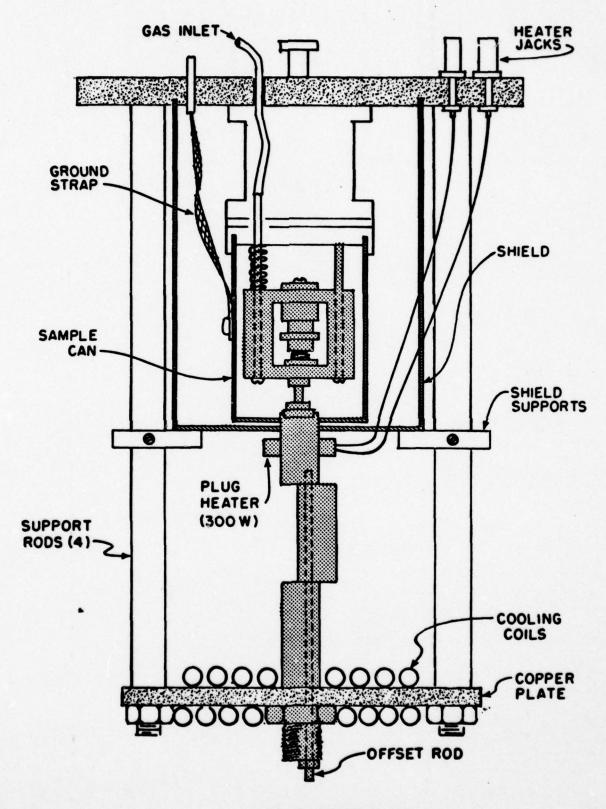
SAMPLE HOLDER AND SAMPLE CAN

Figure 1.



GAS INLET ARRANGEMENT

Figure 2.



DIELECTRIC CELL

Figure 3.

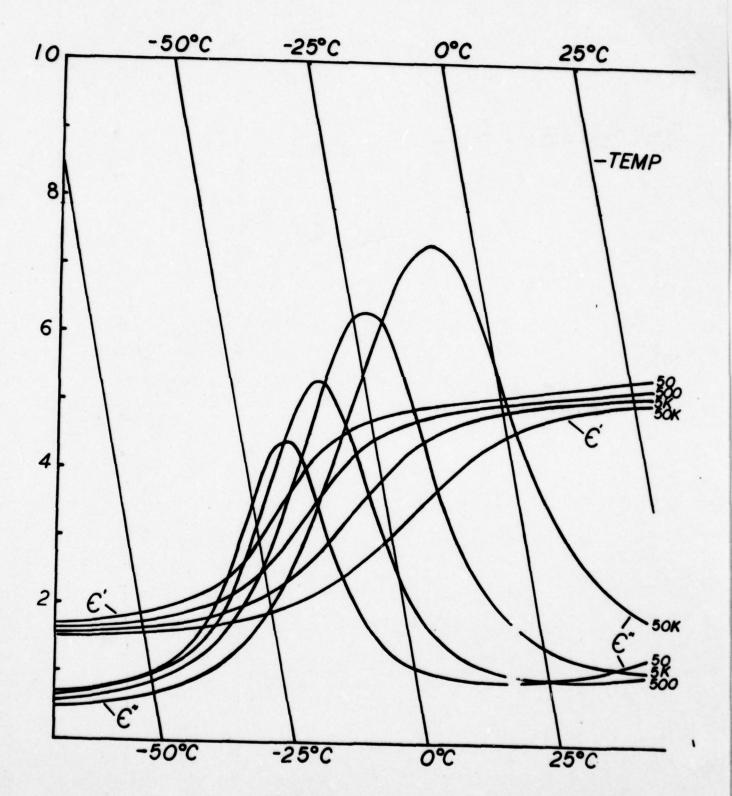


Figure 4.

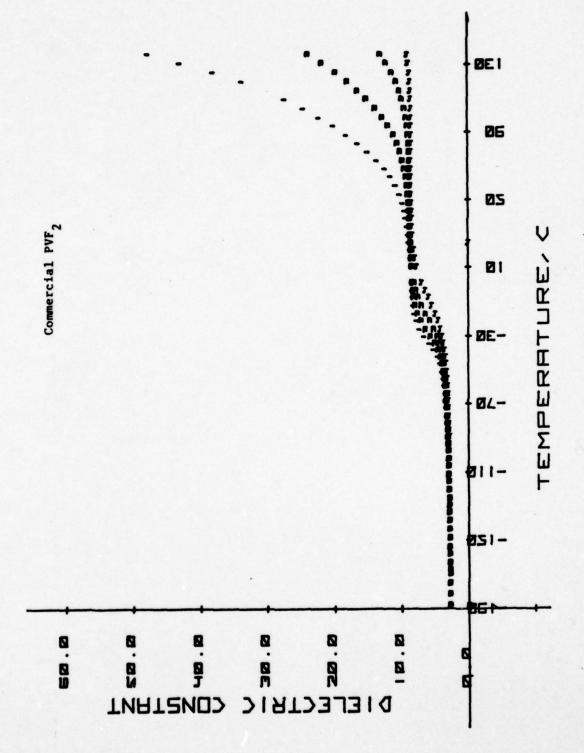
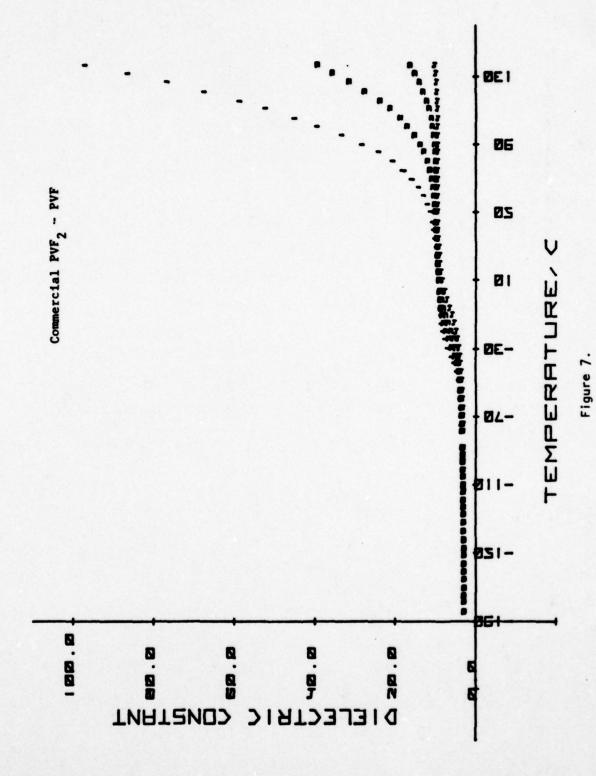


Figure 5.

Figure 6.



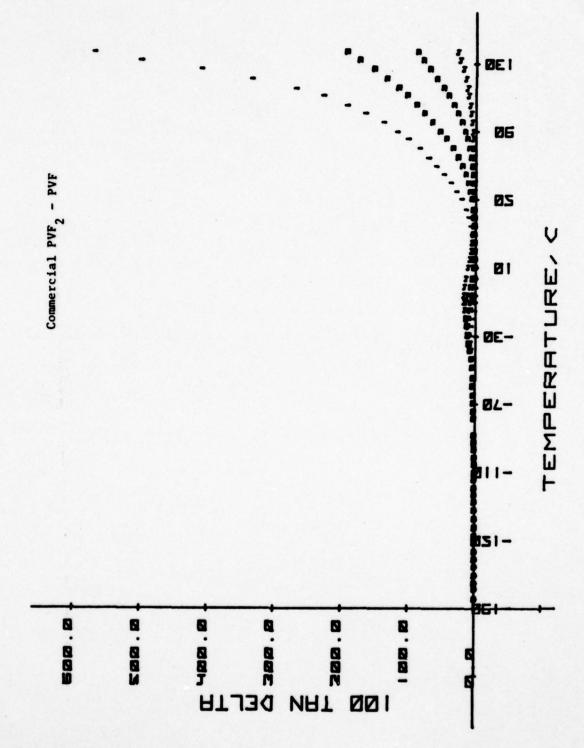


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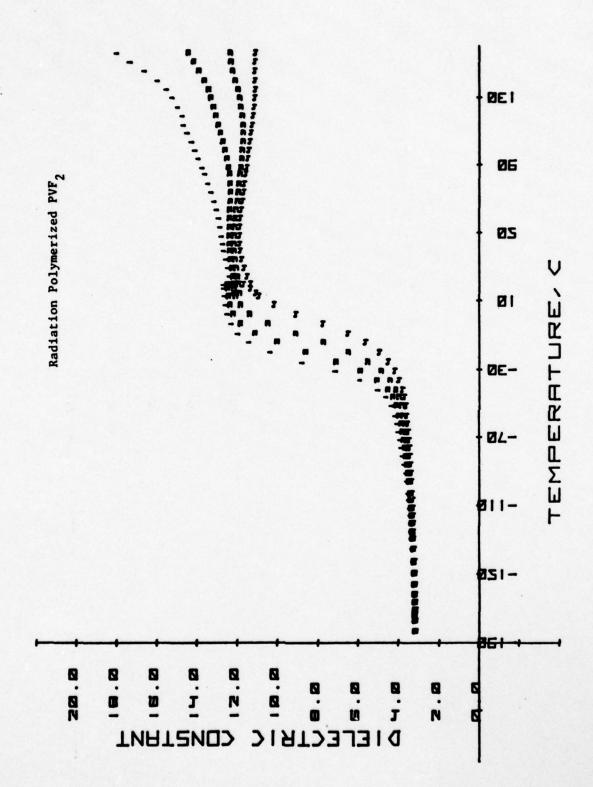


Figure 9.

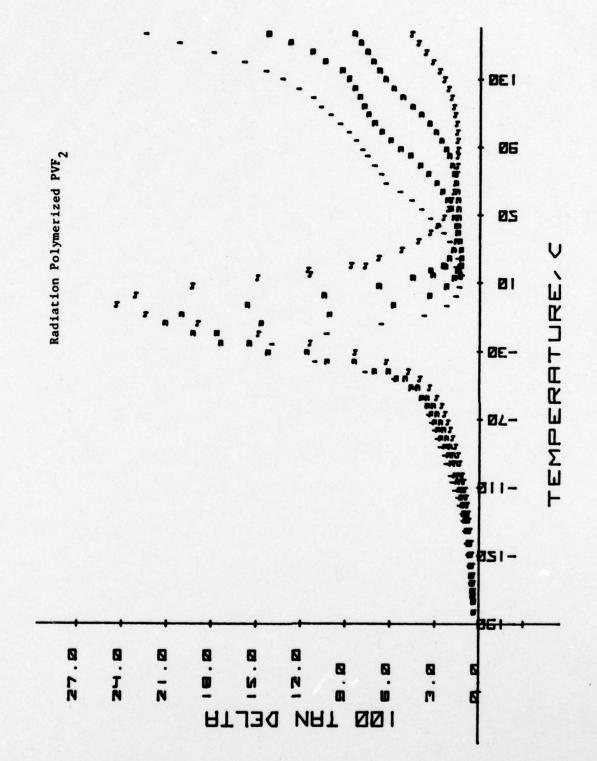


Figure 10.

DIELECTRIC CONST.

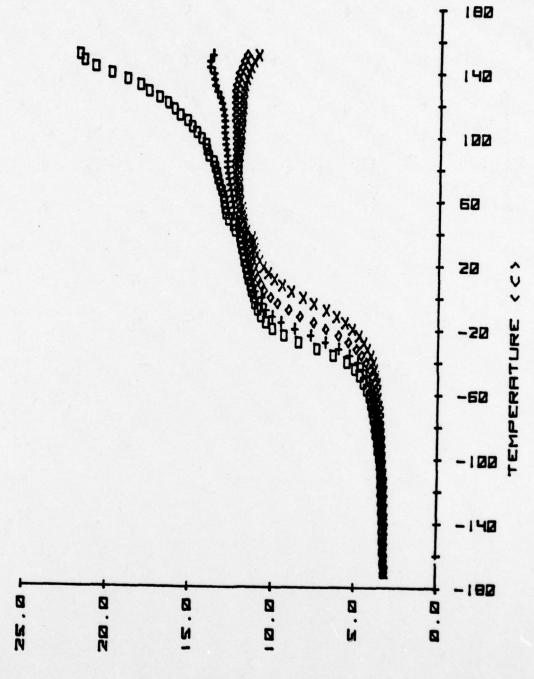


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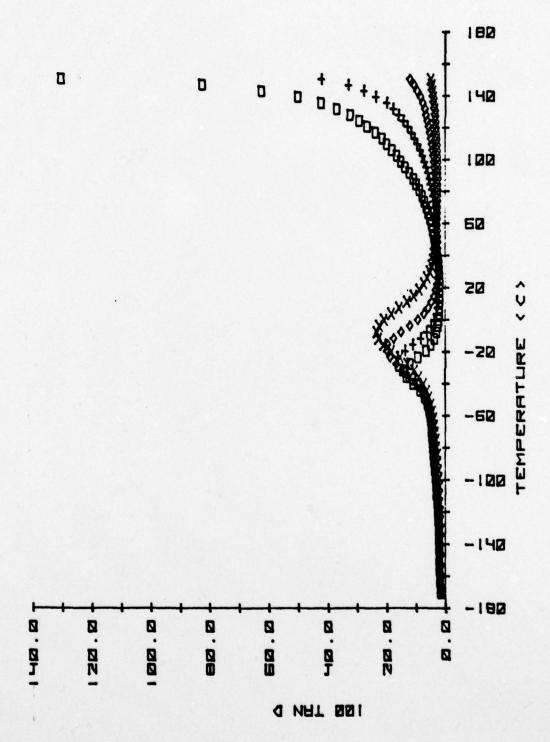
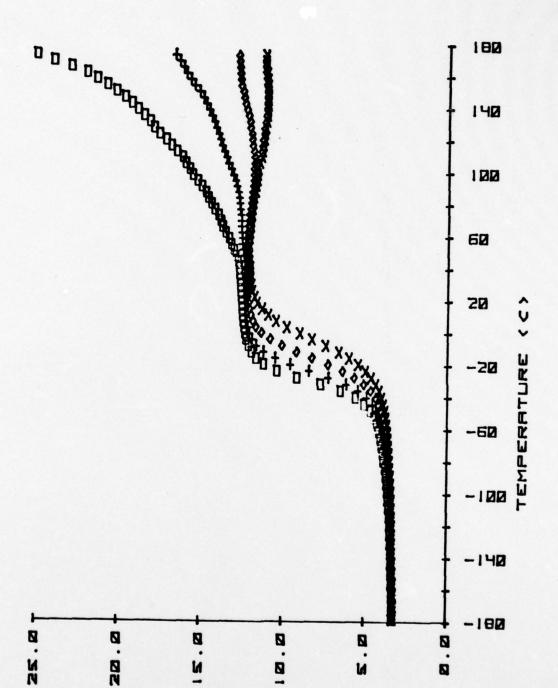


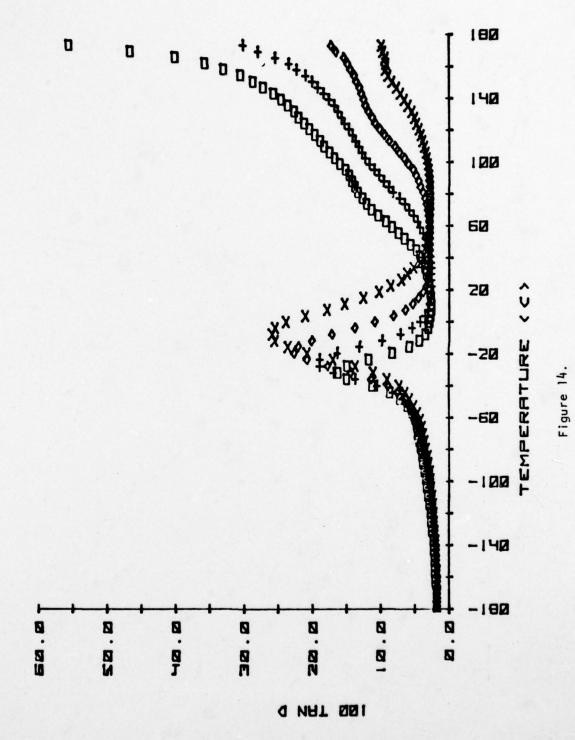
Figure 12.

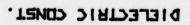


PIELECTRIC CONST.

Figure 13.

180





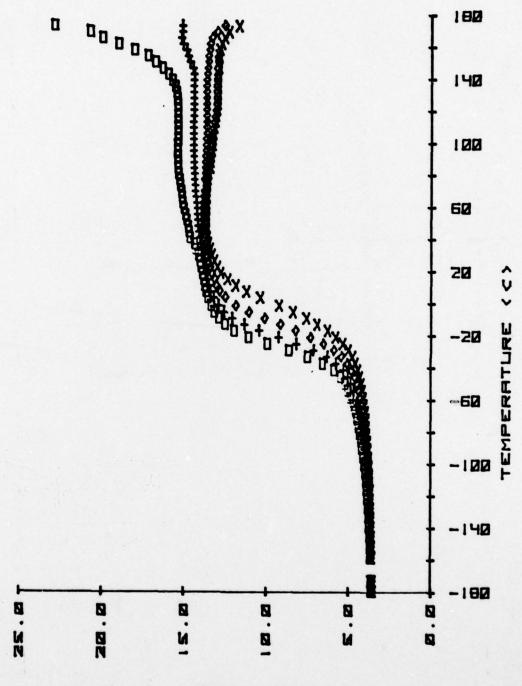
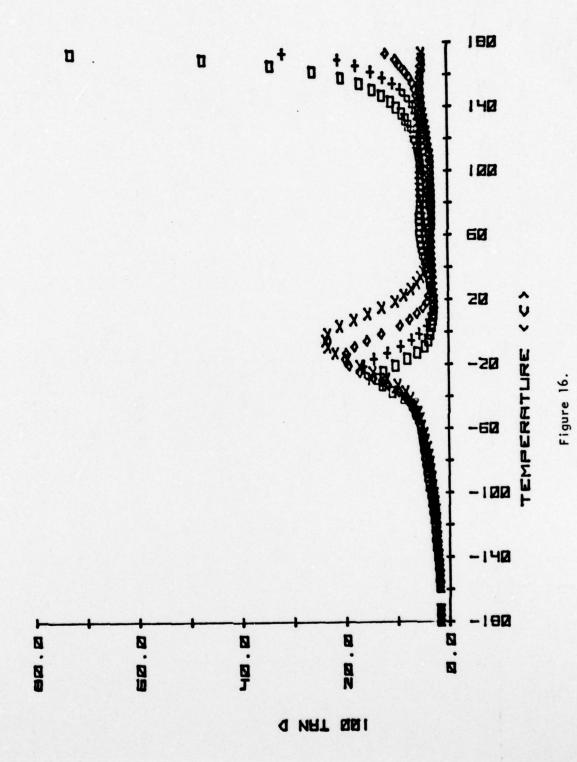
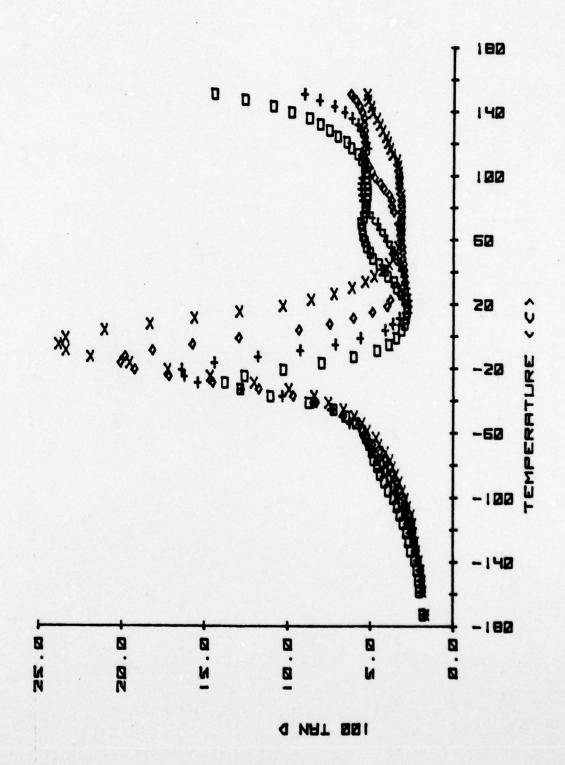


Figure 15.









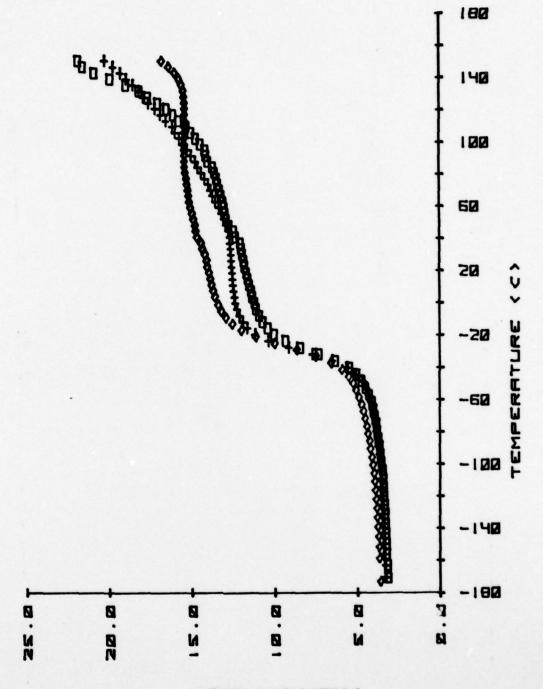


Figure 18.

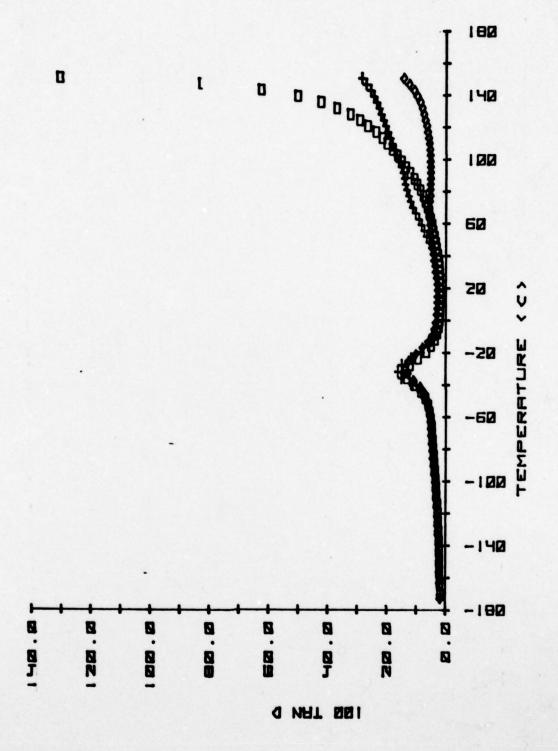


Figure 19.

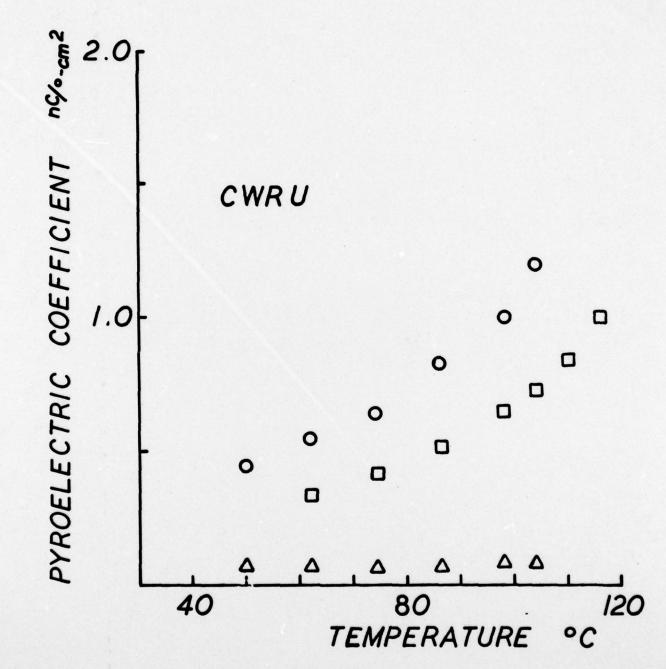


Figure 20.

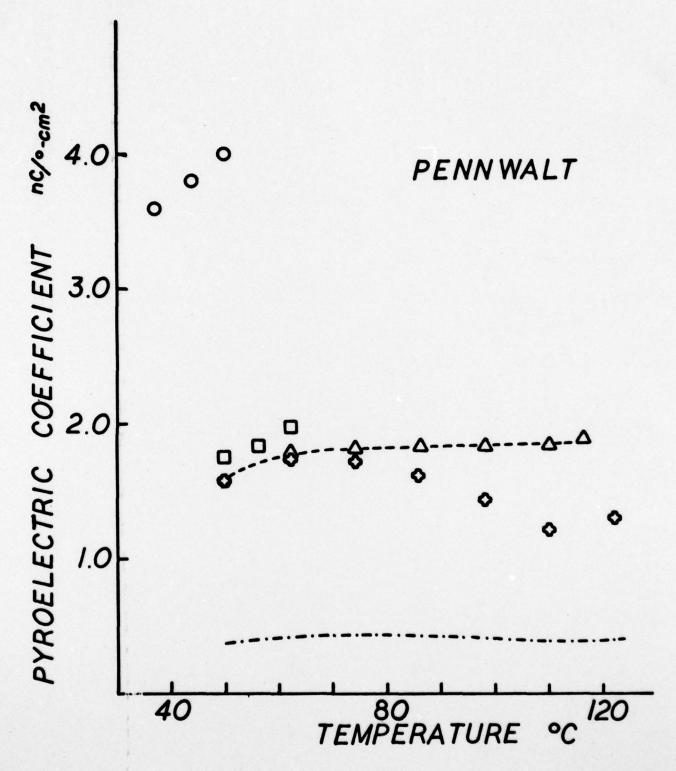


Figure 21.

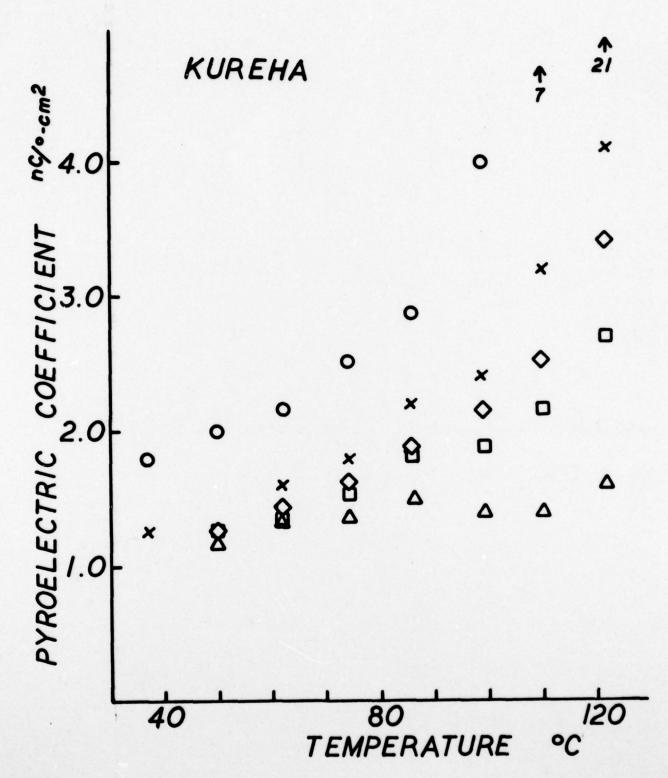


Figure 22.

